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METHOD AND APPARATUS FOR PROVIDING THERMAL SHUTDOWN AND CURRENT LIMITING PROTECTION

INTRODUCTION

Technical Field

This invention pertains to a runaway current and thermal protection method and apparatus, and more particularly to a method and apparatus for reactivating a system once the cause of the runaway current and excessive heat is eliminated.

Background

It has long been known in the prior art to provide thermal shutdown for electronic systems and microchips to prevent the system or chip from generating an excess amount of heat which can damage the system or chip. The generation of excess heat, in one example, is caused when the output load driven by the system is short circuited to ground or low voltage potential which causes the output voltage across the load to drop to substantially zero or the low potential voltage and allow an excess of current to flow through short circuit. This excess current induces a high power dissipation in the system and causes the system to heat up. Protection mechanisms have been developed to prevent the system from continuing to supply the excessive current to the short circuit once the system has reached a predefined temperature. One technique for reactivating a system after thermal shutdown requires the entire system to be powered down and powered up again or re-enabled once the short circuit has been removed. This is time consuming and generally requires user interaction. An alternative technique powers down the system and begins to monitor the temperature of the

system. Once the system has cooled below a predefined temperature, the system reactivates. However, if the short is still present, the system will quickly heat up again only to be shut off by the thermal shutdown mechanism of the system. The system will continue to transition on and off, utilizing large amounts of power and potentially damaging the system, until the short circuit is removed.

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SUMMARY

The present invention provides an apparatus and method for preventing damage to a system due to excessive heat or current and reactivating the system once the cause of the excess current and resulting heat is removed without requiring excessive amounts of power consumption or powering down the system. The apparatus and method is activated when a runaway current condition exists. In one embodiment the shutdown and reactivation apparatus includes a driving circuit which supplies an output current to a load. If the load is short circuited, the output current is greatly increased resulting in a runaway current condition causing the temperature of the system to increase due to high power dissipation. As a result of the increased temperature, the shutdown and reactivation apparatus is activated by triggering a shutdown signal which deactivates the driving circuit such that the output current is no longer supplied to the load. The shutdown signal activates a charging circuit, which supplies a charging current to the load. A first monitoring circuit is coupled with the load, and configured to monitor an output voltage across the load when the shutdown and reactivation apparatus is in the active state. When the short is removed, the charging current is applied to the load to charge a capacitive load. The first monitoring circuit signals the shutdown and reactivation apparatus to transition to a deactivated state when the output voltage across the capacitive load is at least equal to a predefined voltage threshold. The system is re-activated, the charging circuit is deactivated, and the driving circuit again begins to supply the load with the output current when the shutdown and reactivation apparatus is in the deactivated state.

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In accordance with the teachings of this invention a novel method and structure is taught which provides the thermal protection of a system while further re-activating the system once the cause of the damaging effects is removed without requiring large power drains, without user interaction, and without requiring the system to be re-enabled or powered down.

BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 depicts a block diagram of one implementation of one embodiment of the novel thermal and current shutdown protection circuit of the present invention;

5 Fig. 2 shows a block diagram of an alternative implementation of one embodiment of thermal and current shutdown circuit incorporated within the system;

Fig. 3 depicts a schematic diagram of one embodiment of an alternative implementation of shutdown and reactivation circuit of the present invention;

10 Fig. 4 shows one embodiment of a simplified timing diagram of the operation of the shutdown and reactivation circuit depicted in FIG. 3 when the shutdown signal is activated;

Fig. 5 shows one embodiment of a simplified timing diagram of the operation of the deactivation of the shutdown and reactivation circuit and the reactivation of the system;

Fig. 6 depicts a flow diagram of one embodiment of the method of providing thermal shutdown protection and current limit protection of the present invention for preventing damaging effects to a system; and

Fig. 7 depicts a block diagram of an alternative embodiment of the shutdown circuit.

DETAILED DESCRIPTION

The present invention provides for a thermal shutdown and current limiting protection mechanism, apparatus and method for preventing damage to a system due to excessively large current or high power dissipation causing a system or microchip to overheat. The present invention provides for the reactivation of the system once the cause of the excessively large current or high power dissipation has been eliminated. The present invention provides for this reactivation of a system or circuit without powering down the system, without utilizing excessive amounts of power and without further heating of the system. FIG. 1 depicts a block diagram of one implementation of one embodiment of the novel current and thermal shutdown protection and reactivation circuit 120 of the present invention. During normal operation of a system or microchip 121 implementing shutdown and reactivation circuit 120, a driving circuit 124 drives an output load 126. However, if load 126 should happen to be short circuited 130, the output voltage V_{out} will drop and the output current I_{out} supplied by system 121 will drastically increase resulting in a runaway current condition. This increased or runaway output current I_{out} along with the voltage drop across the driving circuit 124 induces high power dissipation. In one embodiment, shutdown and reactivation

5 circuit 120 is activated causing system 120 and output current I_{out} to shutdown if the output current I_{out} exceeds a threshold current level for a predefined period of time. In one embodiment, the higher power dissipation resulting from the increased output current I_{out} causes system 121 to heat up to a predefined threshold temperature causing system 121 to enter current and/or thermal shutdown to prevent damage to system 121. When system 121 enters shutdown, system 121 activates shutdown signal 122 which deactivates driving circuit 124 discontinuing the supply of output current I_{out} to load 126, and activates charging circuit 132. Charging circuit 132 couples a storage element 128 which is configured to generate a voltage potential. In one embodiment the storage element 128 is a capacitive load C_L . In one embodiment, capacitive load C_L is added in parallel with a load 126. In an alternative embodiment, capacitive load C_L is a capacitance existing within the load being driven by system 121.

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15 Still referring to FIG. 1, in one embodiment, charging circuit 132 supplies a small charging current I_C , relative to output current I_{out} conducted through short circuit 130, to load 126. Charging current I_C supplied by charging circuit 132 is maintained at a sufficiently low level so as to allow the temperature of system 121 to decrease while load 126 is still short circuited. The size of charging current I_C is determined by design parameters including size of capacitive load C_L and desired recovery time of system 121. Because charging current I_C is maintained at a relatively small level, shutdown and reactivation circuit 120 requires only a small amount of power to supply the small charging current I_C . Further, because charging current I_C is maintained at a low level, charging current I_C has only minor effects on the rate of temperature dissipation for system 121, allowing the temperature of system 121 to be brought back down to acceptable levels for normal operation. Due to the short circuit, the charging current I_C passes through the short. Once short circuit 130 is eliminated and the 20 runaway current condition has been eliminated, charging current I_C is supplied to capacitive load C_L charging capacitive load C_L . Monitoring circuit 134 monitors the voltage across the capacitive load C_L . Once the output voltage V_{out} across capacitive load C_L exceeds a predefined voltage threshold, monitoring circuit 134 is triggered. Once triggered, monitoring circuit 134 deactivates charging circuit 132, halting charging current I_C , and activating driving circuit 124 to again supply load 126 with output current I_{out} as dictated by system 121 under normal operating conditions.

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Thus, system 121 is reactivated to operate under normal conditions without large power drains, toggling the system off and on causing further over heating of the system and without re-enabling or powering down the system. In one embodiment, driving circuit 124 cannot be reactivated to supply output current I_{out} to load 126 until the temperature of system 121 has been decreased below at least a lower operating temperature threshold. In one embodiment, driving circuit 124 cannot be reactivated until both shutdown signal is transition to a state designating the temperature of system 121 is within operating limits and monitoring circuit 134 detects the elimination of short 130 and the runaway current condition, and signals driving circuit 124.

Charging circuit 132 in combination with capacitive load C_L prevents the need for deactivating or powering down system 121. When signaled to shutdown system 121 is put in a standby mode until signaled by shutdown and reactivation circuit 120 that load 126 is no longer shorted and system 121 can continue to operate as normal.

The desired response time of shutdown and reactivation circuit 120 is dependent on the size of charging current I_C and the size of capacitive load C_L . The shorter the response time desired, the greater the charging current I_C which must be supplied to capacitive load C_L to rapidly charge capacitive load C_L to the voltage threshold. In one embodiment, system 121 cannot be activated until the system 121 temperature has fallen below at least the temperature threshold or below a lower reactivation temperature. Further, the size of capacitive load C_L also affects the response rate at which shutdown and reactivation circuit 120 is deactivated and system 121 is reactivated. The larger the capacitive load C_L , the slower the response time to reactivate system 121. Therefore, the response time is dictated by design parameters, including at least the size of charging current I_C , the size of capacitive load C_L and the temperature dissipation rate of system 121.

In one embodiment, shutdown and reactivation circuit 120 includes a memory device (see FIG. 2), for example a latch or register, to allows a user to program or define the amount of charging current I_C to be supplied to capacitive load C_L . This allows user to program shutdown and reactivation circuit 120 to provide a predefined response time based on the capacitive load C_L utilized by user in implementing the present invention. In one embodiment, the memory device, such as a register, includes a plurality of pins such that user activates a first pin to obtain a first predefined charging current I_C at a first current level and a second pin to obtain a second predefined charging current I_C at a second current level.

One example of a system 121 which is optimized by implementing the present shutdown and reactivation circuit 120 is a Universal Serial Bus (USB) power distribution applications/systems for use in a portable personal computer (PC) or USB hubs.

The shutdown and reactivation apparatus and method of the present invention is capable of being implemented in any system and microchip which includes temperature and/or current shutdown capabilities including PCMCIA Power Controllers, Linear or Switching Regulators, Power Management, Motor Controllers, and any other system and chip implementing temperature and current shutdown.

In one embodiment, shutdown and reactivation circuit 120 is external to and electrically coupled with system 121 to operate in cooperation with system 121, thus allowing shutdown and reactivation circuit 120 to be incorporated with preexisting systems as well as any new system. In an alternative embodiment, shutdown and reactivation circuit 120 is incorporated into system 121 to provide thermal and current protection and reactivation.

FIG. 2 shows a block diagram of one implementation of one embodiment of shutdown and reactivation circuit 120 incorporated within system 121. In the embodiment depicted in FIG. 2, shutdown and reactivation circuit 120 includes a latch 140 for maintaining the driving circuit 124 and charging circuit 132 in an active or deactivate state depending on whether shutdown and reactivation circuit 120 is active or deactivate as described above and more fully below. In one embodiment, latch 140 also allows user to define the desired charging current I_C supplied to capacitive load C_L as described above. Shutdown and reactivation circuit 120 depicted in FIG. 2 further includes a first and second monitoring circuit, 134a and 134b, for monitoring output voltage V_{out} and shutdown signal 122, respectively. Thus, when shutdown signal 122 is activated, second monitoring circuit 134b recognizes the transition and signals latch 140 which receives shutdown signal 122 and registers or latches output levels 142a and 142b to both the driving circuit 124 and the charging circuit 132, respectively. Output levels 142a-b are maintained by latch 140, thus maintaining driving circuit 124 in an inactive state and charging circuit 132 in an active state, until output voltage V_{out} across capacitive load C_L reaches the predefined voltage threshold to activate first monitoring circuit 134a. First monitor circuit 134 then signals latch 140 which latches output levels 142a-b to reactivate driving circuit 124 and to deactivate charging circuit 132. In one embodiment, shutdown and reactivation circuit 120 includes register 143 coupled with charging circuit 132. Register 143 allows user to program shutdown and reactivation circuit

120 to provide a predefined charging current I_C to capacitive load C_L . Register 143 signals charging circuit 132 to supply charging current I_C at one of a plurality of current levels. In one embodiment, register 143 is included within charging circuit to allow a user to program charging circuit 132.

5 FIG. 3 depicts a schematic diagram of one embodiment of an alternative implementation of shutdown and reactivation circuit 120. Shutdown signal 122 is directed through second monitoring circuit 134b including a series of inverters INV₉ and INV₁₀ coupled with a first edge detector 144a which detects a change in shutdown signal 122. In one embodiment, first edge detector 144a includes a first NAND gate ND₁ which has a first and second input, A₁ and B₁, respectively. First input A₁ receives an output signal from inverter INV₁₀ and second input B₁ receives an output from three inverters INV₁₁, INV₁₂ and INV₁₃ coupled in series. First edge detector 144a forwards the change in shutdown signal 122 through inverter INV₁₄ to a set-input S of flip-flop 150.

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Still referring to FIG. 3, in one embodiment, first monitoring circuit 134a further includes a string of inverters INV₁, INV₂, INV₃ and INV₄ coupled in series supplying a threshold signal 146 to a second edge detector 144b. In one embodiment, second edge detector 144b includes a second NAND gate ND₂ which receives an output from inverter INV₄ as a first input A₂ and an output from three inverters INV₅, INV₆ and INV₇, coupled in series as a second input B₂. Second edge detector 144b forwards a signal through inverter INV₈ which in turn supplies a signal to a reset-input R of flip-flop 150.

25 In one embodiment, flip-flop 150 further includes a first and second output Q and QB, where second output QB is the inverse of first output Q. First flip-flop output Q activates and deactivates driving circuit 124, and second flip-flop output QB activates and deactivates charging circuit 132. In one embodiment, driving circuit 124 includes a switch 152 which switches driving circuit 124 between the active state to supply output current I_{out} to load 126, and a deactivated state preventing output current I_{out} from being supplied to load 126. In one embodiment, switch 152 consists of a first Nch transistor MN1 and a second Nch transistor MN2, where first Nch transistor MN1 receives first flip-flop output Q. When shutdown signal 122 has not been activated and system is operating under normal conditions, first flip-flop output Q is in a low state, deactivating first Nch transistor MN1, which allows second Nch transistor MN2 to operate in an active state supplying output current I_{out} to load 126. Second Nch transistor MN2 is further coupled with a gate drive 154. Gate drive 154 controls

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the level of output current I_{out} supplied through second Nch transistor MN2 to load 126, as dictated by system 121. Second flip-flop output QB couples with charging circuit 132 to activate and deactivate charging circuit 132. In one embodiment, charging circuit 132 includes a first Pch transistor MP1. When system 121 is operating under normal operating conditions, second flip-flop output QB is in a high state, thus, MP1 is off and charging circuit 132 is in a deactivated state. First Pch transistor MP1 is activated when shutdown signal 122 is triggered, which is latched through flip-flop 150 causing Q to transition high and QB to transition low. When Q transitions high, first Nch transistor MN1 of driving circuit 124 is activated pulling node N1 low effectively deactivating second Nch transistor MN2 and thus deactivating driving circuit 124. Once in a deactivated state, driving circuit 124 prevents output current I_{out} from being supplied to load 126. When QB transitions low, charging circuit 132 is activated, activating first Pch transistor MP1 to supply charging current I_C to capacitive load C_L .

Referring to FIGS. 3 and 4, FIG. 4 shows one embodiment of a simplified timing diagram of the operation of the shutdown and reactivation circuit 120 depicted in FIG. 3 when shutdown signal 122 is activated resulting in the deactivation of driving circuit 124 and activation of charging circuit 132. At time T_0 , system 121 and shutdown and reactivation circuit 120 are inactive. At time T_1 , system 121 is activated, driving circuit 124 begins to supply output current I_{out} to load 126 and output voltage V_{out} ramps up across load 126. At time T_2 , load 126 is short circuited causing the output voltage V_{out} to drop, the output current I_{out} to jump up to a high level, and the power dissipation to increase driving the system 121 into shutdown. In one embodiment, if the temperature of the system exceeds a temperature threshold, system 121 almost immediately triggers shutdown signal 122 to transition at time T_3 activating shutdown circuit 120.

In one embodiment, if the output current I_{out} exceeds a predefined threshold current for a predefined time delay t_D , system 121 triggers the shutdown signal 122 at time T_3 , where time T_3 is delayed by time t_D . In one embodiment, delay time t_D is incorporated within system 121, or alternatively in shutdown circuit 120, to avoid deactivating driving circuit 124 in the event of glitching, current or voltage spikes, as well as during power-up and power-down procedures of system 121 and shutdown and reactivation circuit 120. This delayed time t_D ensures that shutdown and reactivation circuit 120 is activated upon valid overcurrent conditions and that erroneous error reporting and shutdowns are eliminated. Triggered

shutdown signal 122 passes through inverters INV₉ and INV₁₀ which speed up the signal edge of shutdown signal 122 and subsequently is inputted to first edge detector 144a. The input to first edge detector 144a is conducted directly to first input A₁ of first NAND gate ND₁ and is further passed through the series of inverters INV₁₁ - INV₁₃ to be supplied to second input B₁ of first NAND gate ND₁. Because of the delay caused by the series of inverters INV₁₁ - INV₁₃ forwarding the signal to second input B₁, both first input A₁ and second input B₁ are in a high state between times T₄ and T₆. These high states in both A₁ and B₁ cause first NAND gate ND₁ to output a low state signal 160 at T₄ until the input signal 148 of first edge detector 144a propagates through the series of inverters INV₁₁ - INV₁₃ to transition second input B₁ low at time T₆. Thus, first edge detector 144a detects the transition of shutdown signal 122 and generates a low pulse 160 through first NAND gate ND₁. Low pulse 160 generated by first edge detector 144a is forwarded through inverter INV₁₄ to supply a high pulse 162 to set-input S of flip-flop 150 causing first output Q to transition to a high state. The transition of first flip-flop output Q shuts off driving circuit switch 152 deactivating driving circuit 124 by activating first Nch transistor MN1 which in turn shuts-off second Nch transistor MN2, thus, output current I_{out} is turned off. High pulse 162 at set-input S further causes second output QB to transition low activating first Pch transistor MP1 of charging circuit 132 to produce charging current I_C.

Flip-flop 150 maintains this state, Q in a high state and QB in a low state, until short circuit 130 is eliminated and output voltage V_{out} across capacitive load C_L is charged by charging current I_C to the threshold level of inverter INV₁. It will be apparent to one skilled in the art that the levels of the states can be reversed and the threshold levels altered without departing from the novelty of the invention.

Referring to FIGS. 3 and 5, FIG. 5 shows one embodiment of a simplified timing diagram of the operation of shutdown and reactivation circuit 120 depicted in FIG. 3 when capacitive load C_L is charged to the threshold level of inverter INV₁ and shutdown signal 122 is deactivated. At time T₉, system 121 (not shown) and shutdown and reactivation circuit 120 are in the shutdown state as described in reference to FIG. 4 at time T₈. At Time T₁₀ short circuit 130 and load 126 are removed causing shutdown signal to transition low. At time T₁₁ output voltage V_{out} across capacitive load C_L reaches the threshold level of inverter INV₁. The transition at the input of inverter INV₁ from low to high is propagated through the series of inverters INV₁ - INV₄ speeding up the signal edge and provide the input signal to second

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edge detector 144b. Thus, first input A_2 of second NAND gate ND_2 receives the transition of signal 146 from low to high following the delay through inverters INV_1 - INV_4 at time T_{13} . The input to second edge detector 144b is further propagated through the series of inverters INV_5 - INV_7 to transition second input B_2 of second NAND gate ND_2 at time T_{15} . Because both inputs A_2 and B_2 of second NAND gate ND_2 are in a high state between times T_{13} and T_{15} , second edge detector 144b generates a low pulse 164. Low pulse 164 is inverted through inverter INV_8 which supplies a high pulse 166 to reset-input R of flip-flop 150 resetting flip-flop 150. Thus, first output Q of flip-flop 150 transitions from high to low 168 reactivating driving circuit 124, and second output QB transitions from low to high 170 deactivating charging circuit 132. The reactivation of driving circuit 124 reinitializing system 121 to drive output load 126 through driving circuit 124 without the need to reset or re-enable either system 121 or shutdown and reactivation circuit 120. Further, system 121 is reactivated without requiring shutdown and reactivation circuit 120 to continuously toggle on and off to determine when the short circuit 130 is removed, avoiding continued heating of system 121, and further avoiding the increased power consumption of the prior art.

FIG. 6 depicts a flow diagram of one embodiment of the method of providing thermal and current limit protection with system reactivation of the present invention for preventing damaging effects to a system. Initially in step 250, system 121 is operating under normal conditions such that output current I_{out} is supplied through driving circuit 124 to load 126 and load 126 is not short circuited. In step 252, it is determined whether output current I_{out} has exceeded predefined limits I_{Lim} or thermal threshold has been exceeded signaling shutdown and reactivation circuit 120. If thermal and/or output current thresholds have not been exceeded, then the process returns back to step 250 such that system 121 continues to operate normally. If thermal or output current thresholds have been exceeded, then step 254 is entered where shutdown signal 122 is activated. In step 256, shutdown and reactivation circuit 120 deactivates driving circuit 124 to shutdown output current I_{out} . In step 260, charging circuit 132 is activated to supply capacitive load C_L with charging current I_C . In step 262, shutdown and reactivation circuit 120 monitors output voltage V_{out} . In step 264, shutdown and reactivation circuit 120 determines if output voltage exceeds a predefined threshold designating that short circuit 130 has been removed. If not, the process returns to step 262 where shutdown and reactivation circuit 120 continues to monitor output voltage V_{out} . If output voltage V_{out} exceeds the predefined threshold, the process shifts to step 266

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where driving circuit 124 is reactivated to again begin to supply load 126 with output current I_{out} . In step 270, charging circuit 132 is deactivated shutting off charging current I_C and returning system 121 and process to step 250 for normal operation.

FIG. 7 depicts a block diagram of one embodiment of shutdown and reactivation circuit 120. Shutdown signal 122 couples with first edge detector 310 through a pair of series coupled inverters INV₅₀ and INV₅₁. First edge detector 310 registers the assertion of the shutdown signal 122 and outputs a pulse through inverter INV₅₂ to a set-input S of latch 312. The pulse at set-input S of latch 312 reverses the states of first latch output Q and second latch output QB. The transition of first output Q deactivates driving circuit 124 (not shown) thus preventing the flow of output current I_{out} through short circuit 130 (not shown) and prevents further power dissipation and heating of system 121. The transition of second output QB activates charging circuit 132 to supply the small charging current I_C to load 126 (not shown). Once short circuit 130 has been eliminated, charging current I_C charges capacitive load C_L (not shown) increasing output voltage V_{out} . Once output voltage V_{out} reaches a threshold level of inverter INV₅₄, inverter INV₅₄ forwards a signal through the series of inverters INV₅₅, INV₅₆ and INV₅₇ to second edge detector 314. Second edge detector 314 detects the pulse signaling the removal of short circuit 130 and outputs a signal to reset-input R of latch 312 through NAND gate 316. Latch 312 is reset causing outputs Q and QB to transition to opposite states reactivating driving circuit 124 (not shown) and deactivating charging circuit 132. In one embodiment, NAND gate 316 is a three input NAND gate receiving not only the pulse from second edge detector 314, but also the transition of an enable signal 320 through third edge detector 322, and a cycling supply signal 324 from a power-on-reset 326 through inverter INV₅₈ to provide further control over shutdown and reactivation circuit 120.

The invention now being fully described, it will be apparent to one of ordinary skill in the art that many changes and modifications can be made thereto without departing from the spirit or scope of the appended claims.